DATA SHEET

TEA1507

GreenChip™II SMPS control IC

Preliminary specification   2000 Nov 14
File under Integrated Circuits, IC11

Philips
Semiconductors

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GreenChip™II SMPS control IC

TEA1507

FEATURES

Distinctive features

- Universal mains supply operation (70 to 276 V AC)
- High level of integration, giving a very low external component count.

Green features

- Valley/zero voltage switching for minimum switching losses
- Efficient quasi-resonant operation at high power levels
- Frequency reduction at low power standby for improved system efficiency (<3 W)
- Burst mode operation for very low standby levels (<1 W)
- On-chip start-up current source.

Protection features

- Safe restart mode for system fault conditions
- Continuous mode protection by means of demagnetization detection (zero switch-on current)
- Accurate and adjustable overvoltage protection
- Short winding protection
- Undervoltage protection (foldback during overload)
- Overtemperature protection
- Low and adjustable overcurrent protection trip level
- Soft (re)start
- Mains voltage-dependent operation-enabling level.

APPLICATIONS

Besides typical application areas, i.e. TV and Monitor supplies, the device can be used in all applications that demand an efficient and cost-effective solution up to 250 W.

Fig.1 Typical application.
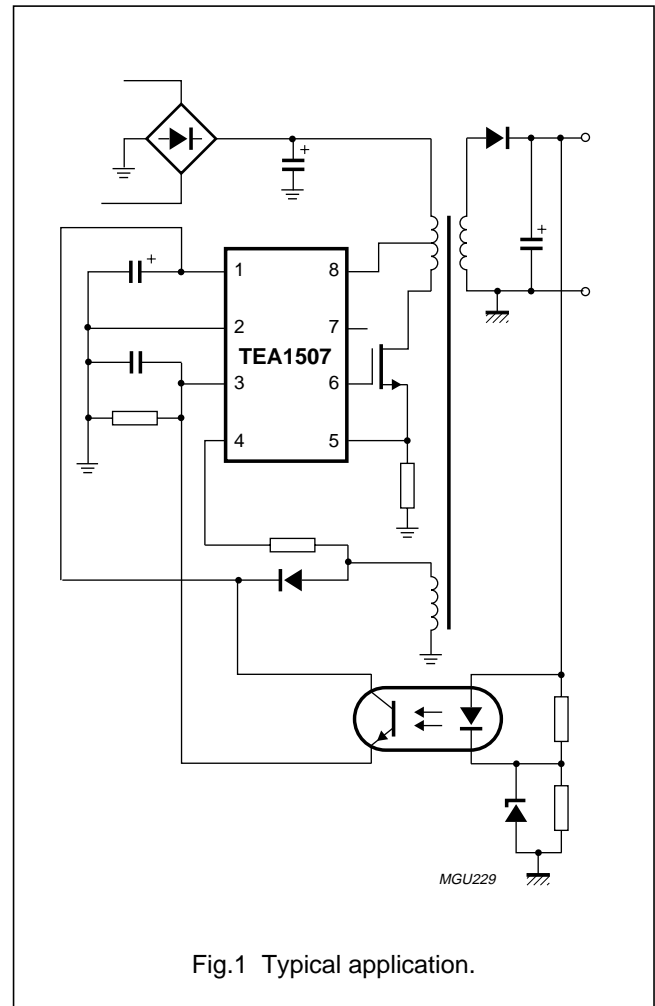
GreenChip™II SMPS control IC   TEA1507

GENERAL DESCRIPTION

The GreenChip™II is the second generation of green Switched Mode Power Supply (SMPS) controller ICs operating directly from the rectified universal mains. A high level of integration leads to a cost effective power supply with a very low number of external components.

The special built-in green functions allow the efficiency to be optimum at all power levels. This holds for quasi-resonant operation at high power levels, as well as fixed frequency operation with valley switching at medium power levels. At low power (standby) levels, the system operates at reduced frequency and with valley detection.

If burst mode operation is applied, the standby power level can even be reduced to below 1 W.

The proprietary high voltage BCD800 process makes direct start-up possible from the rectified mains voltage in an effective and green way. A second low voltage BICMOS IC is used for accurate, high speed protection functions and control.

Highly efficient, reliable supplies can easily be designed using the GreenChip™II controller.

ORDERING INFORMATION

TYPE NUMBER	PACKAGE		
	NAME	**DESCRIPTION**	**VERSION**
TEA1507P	DIP8	plastic dual in-line package; 8 leads (300 mil)	SOT97-1
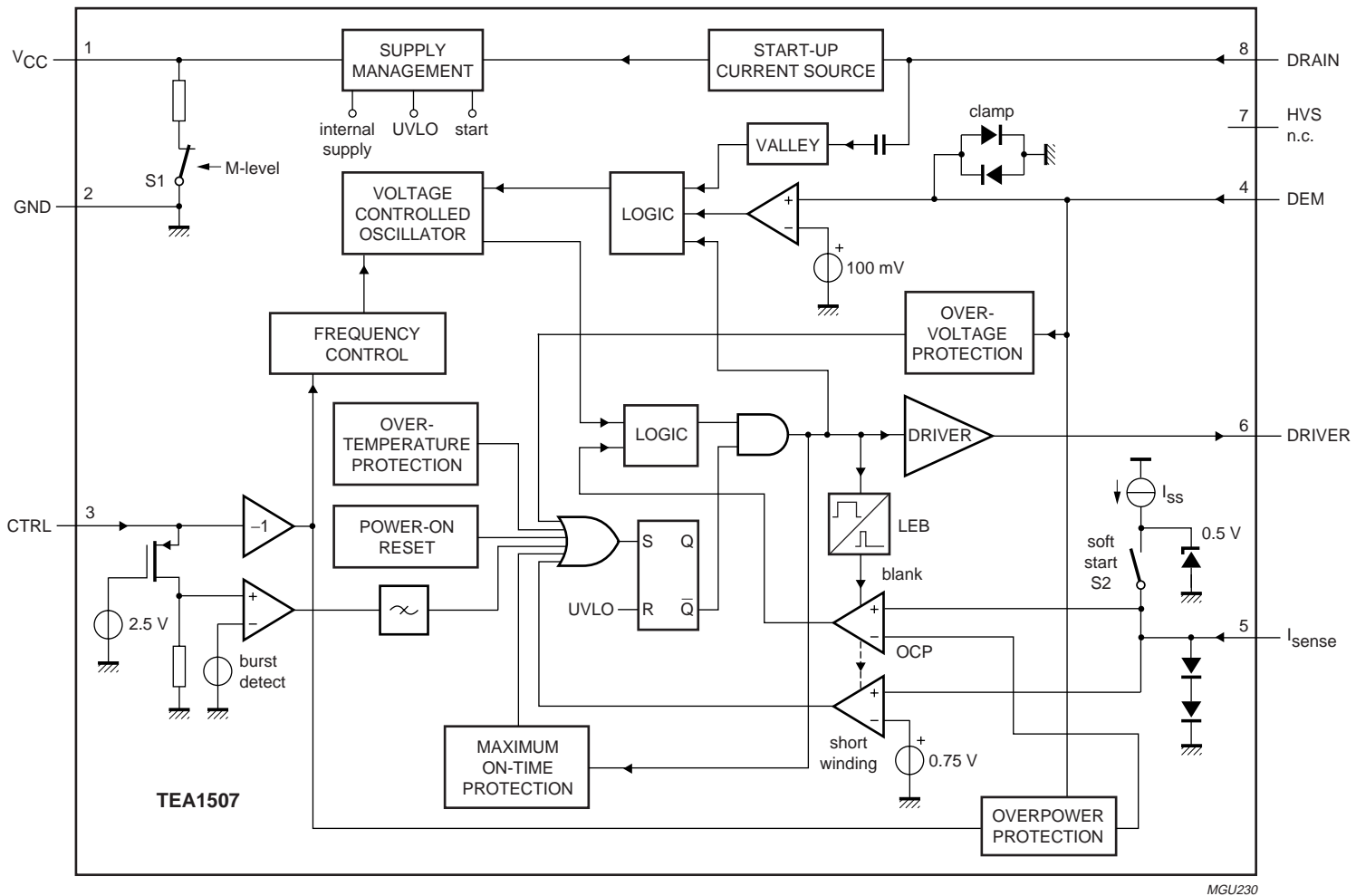
BLOCK DIAGRAM

Fig.2 Block diagram.

MGU230

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TEA1507

PINNING

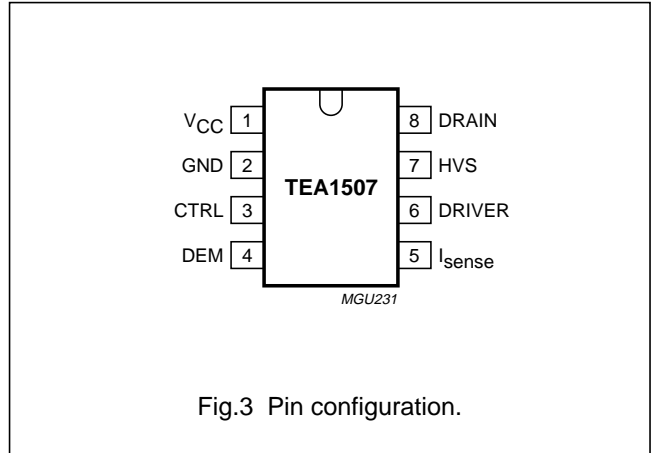| SYMBOL	PIN	DESCRIPTION
V_{CC}	1	supply voltage
GND	2	ground
CTRL	3	control input
DEM	4	input from auxiliary winding for demagnetization timing, OVP and OPP
I_{sense}	5	programmable current sense input
DRIVER	6	gate driver output
HVS	7	high voltage safety spacer, not connected
DRAIN	8	drain of external MOS switch, input for start-up current and valley sensing

Fig.3 Pin configuration.

FUNCTIONAL DESCRIPTION

The TEA1507 is the controller of a compact flyback converter, with the IC situated at the primary side. An auxiliary winding of the transformer provides demagnetization detection and powers the IC after start-up.

The TEA1507 operates in multi modes.

The next converter stroke is started only after demagnetization of the transformer current (zero current switching), while the drain voltage has reached the lowest voltage to prevent switching losses (green function). The primary resonant circuit of primary inductance and drain capacitor ensures this quasi-resonant operation. The design can be optimized in such a way that zero voltage switching can be reached over almost the universal mains range.

To prevent very high frequency operation at lower loads, the quasi-resonant operation changes smoothly in fixed frequency PWM control.

At very low power (standby) levels, the frequency is controlled down, via the VCO, to a minimum frequency of about 6 kHz. Typically, 3 Watts can be achieved for a 75 W converter with an output power of 100 mW.

Start-up, mains enabling operation level and undervoltage lock out (see Figs. 10 and 11)

Initially, the IC is self supplying from the rectified mains voltage via pin DRAIN. Supply capacitor C_{VCC} is charged by the internal start-up current source to a level of about 4 V or higher, depending on the drain voltage. Once the drain voltage exceeds the M-level (mains-dependent operation-enabling level), the start-up current source will

continue charging capacitor C_{VCC} (switch S1 will be opened), see Fig.2. The IC will activate the power converter as soon as the voltage on pin V_{CC} passes the $V_{CC(start)}$ level. The IC supply is taken over by the auxiliary winding as soon as the output voltage reaches its intended level and the IC supply from the mains voltage is subsequently stopped for high efficiency operation (green function).

The moment the voltage on pin V_{CC} drops below the V_{UVLO} (undervoltage lock out) level, the IC stops switching and enters a safe restart from the rectified mains voltage. Inhibiting the auxiliary supply by external means causes the converter to operate in a stable, well-defined burst mode.

Supply management

All (internal) reference voltages are derived from a temperature compensated, on-chip band gap circuit.
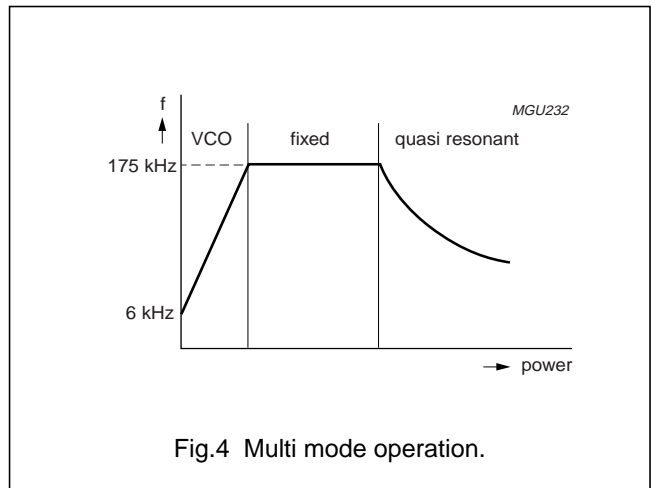

Fig.4 Multi mode operation.

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TEA1507

Current mode control

Current mode control is used for its good line regulation behaviour.

The 'on-time' is controlled by the internally inverted control pin voltage, which is compared with the primary current information. The primary current is sensed across an external resistor. The driver output is latched in the logic, preventing multiple switch-on.

The internal control voltage is inversely proportional to the external control pin voltage, with an offset of 1.5 V. This means that a voltage range from 1 to 1.5 V on pin CTRL will result in an internal control voltage range from 0.5 to 0 V (the maximum external control voltage results in a minimum duty cycle).

Oscillator

The maximum fixed frequency of the oscillator is set by an internal current source and capacitor. The maximum frequency is reduced once the control voltage enters the VCO control window. Then, the maximum frequency changes linearly with the control voltage until the minimum frequency is reached (see Figs 5 and 6).

Valley switching (see Fig.7)

A new cycle starts when the power switch is switched on. After the 'on-time' (which is determined by the 'sense' voltage and the internal control voltage), the switch is opened and the secondary stroke starts. After the secondary stroke, the drain voltage shows an oscillation with a frequency of approximately $\dfrac{1}{(2 \times \pi \times \sqrt{(L_p \times C_d)})}$

where L_p is the primary self inductance of the transformer and C_d is the capacitance on the drain node.

As soon as the oscillator voltage is high again and the secondary stroke has ended, the circuit waits for the lowest drain voltage before starting a new primary stroke. This method is called valley detection. Figure 7 shows the drain voltage together with the valley signal, the signal indicating the secondary stroke and the oscillator signal.

In an optimum design, the reflected secondary voltage on the primary side will force the drain voltage to zero. Thus, zero voltage switching is very possible, preventing large capacitive switching losses $\left(P = \dfrac{1}{2} \times C \times V^2 \times f \right)$, and allowing high frequency operation, which results in small and cost effective inductors.
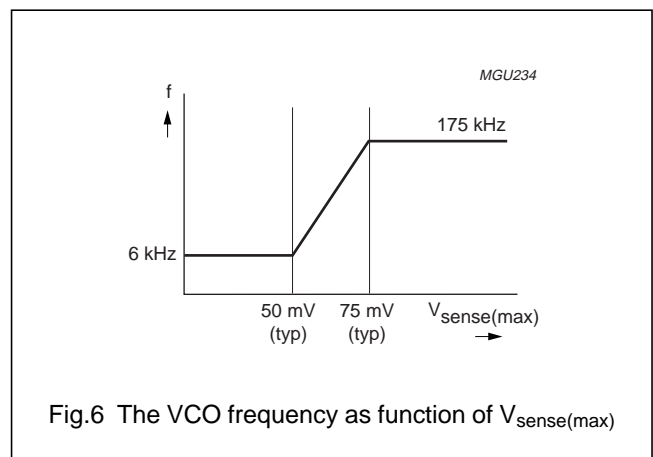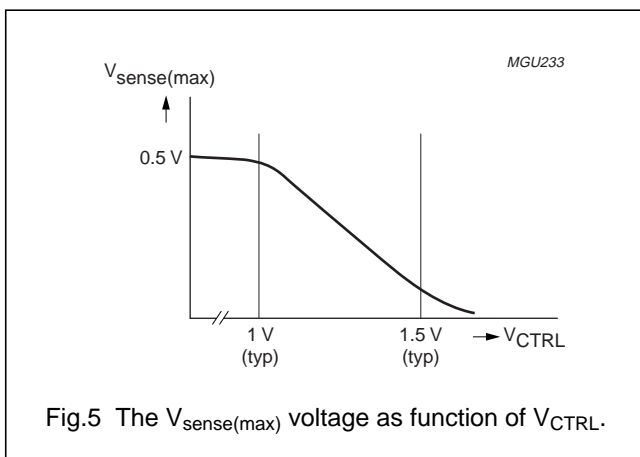
Demagnetization

The system will be in discontinuous conduction mode all the time. The oscillator will not start a new primary stroke until the secondary stroke has ended.

Demagnetization features a cycle-by-cycle output short-circuit protection by immediately lowering the frequency (longer off-time), thereby reducing the power level.

Demagnetization recognition is suppressed during the first t_{suppr} time. This suppression may be necessary in applications where the transformer has a large leakage inductance and at low output voltages/start-up.

Minimum and maximum 'on-time'

The minimum 'on-time' of the SMPS is determined by the Leading Edge Blanking (LEB) time. The IC limits the 'on-time' to 50 μs. When the system desires an 'on-time' longer than 50 μs, a fault condition is assumed (e.g. removed C_i), the IC will stop switching and enter the safe restart mode.

MGU233

Fig.5 The $V_{sense(max)}$ voltage as function of V_{CTRL}.

MGU234

Fig.6 The VCO frequency as function of $V_{sense(max)}$

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primary stroke

secondary stroke

secondary ringing

drain

valley

secondary stroke

oscillator

B   A
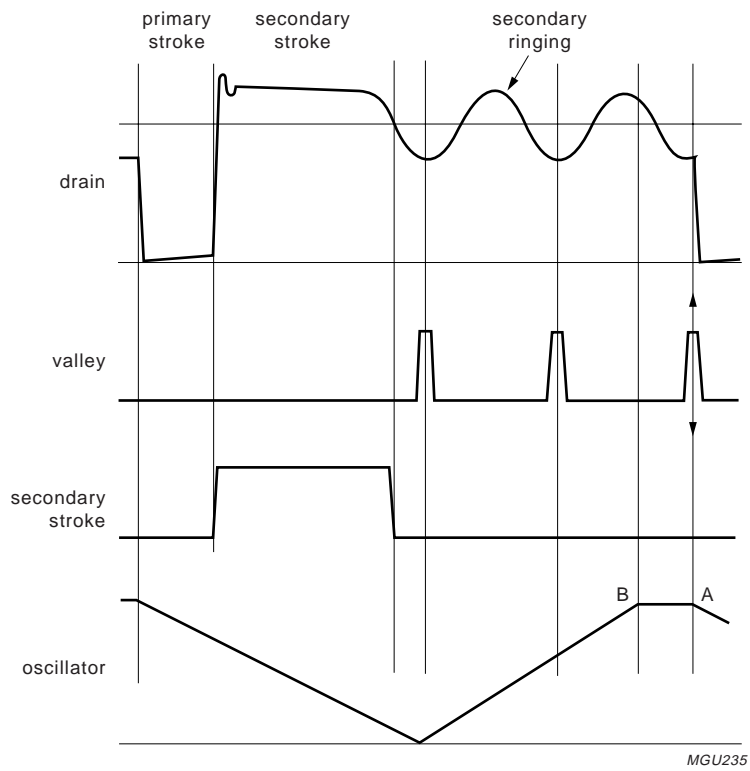
MGU235

A: Start of new cycle at lowest drain voltage.

B: Start of new cycle in a classical PWM system at high drain voltage.

Fig.7 Signals for valley switching.

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OverVoltage Protection (OVP)

An OVP mode is implemented in the GreenChip™ series. For the TEA1507, this works by sensing the auxiliary voltage via the current flowing into pin DEM during the secondary stroke. The auxiliary winding voltage is a well-defined replica of the output voltage. Any voltage spikes are averaged by an internal filter.

If the output voltage exceeds the OVP trip level, the OVP circuit switches the power MOSFET off. Next, the controller waits until the UVLO level is reached on pin V_{CC}. This is followed by a safe restart cycle, after which switching starts again. This process is repeated as long as the OVP condition exists.

The output voltage at which the OVP function trips, $V_{o(OVP)}$ can be set by the demagnetization resistor, R_{DEM}:

$$V_{o(OVP)} = \frac{N_s}{N_{aux}} \times (I_{(OVP)(DEM)} \times R_{DEM} + V_{clamp(DEM)(pos)})$$

Where N_s is the number of secondary turns and N_{aux} is the number of auxiliary turns of the transformer.

Current I_{ref} is internally trimmed.

The value of the demagnetization resistor (R_{DEM}) can be adjusted to the turns ratio of the transformer, thus making an accurate OVP possible.

OverCurrent Protection (OCP)

The cycle-by-cycle peak drain current limit circuit uses the external source resistor to measure the current accurately. This allows optimum size determination of the transformer core (cost issue). The circuit is activated after the leading edge blanking time, t_{leb}. The OCP protection circuit limits the 'sense' voltage to an internal level.

OverPower Protection (OPP)

During the primary stroke, the rectified mains input voltage is measured by sensing the current drawn from pin DEM. This current is dependent on the mains voltage, according to the following formula: $I_{(DEM)} \approx \dfrac{V_{aux}}{R_{DEM}} \approx \dfrac{N \times V_{mains}}{R_{DEM}}$

Where: $N = \dfrac{N_{aux}}{N_p}$

The current information is used to adjust the peak drain current, which is measured via pin I_{sense}. The internal compensation is such that an almost mains independent maximum output power can be realized.

The OPP curve is given in Fig.8.

Fig.8 OPP correction curve.
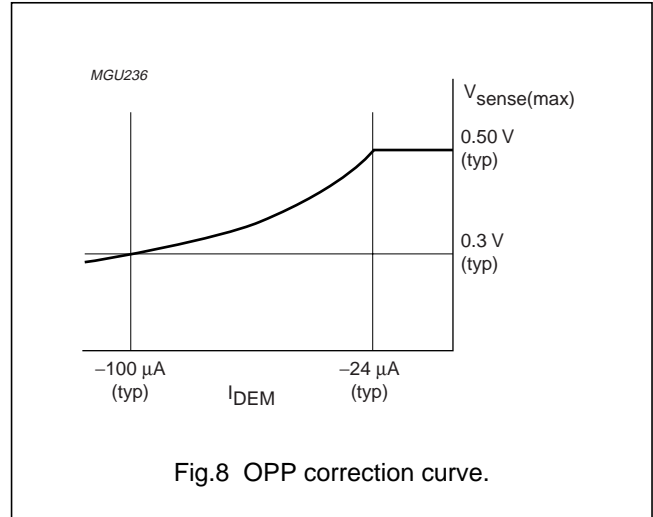
Short winding protection

After the leading edge blanking time, the short winding protection circuit is also activated. If the 'sense' voltage exceeds the short winding protection voltage V_{swp}, the converter will stop switching. Once V_{CC} drops below the UVLO level, capacitor C_{VCC} will be recharged and the supply will restart again. This cycle will be repeated until the short circuit is removed (safe restart mode).

The short winding protection will also protect in case of a secondary diode short circuit.

Overtemperature protection

An accurate temperature protection is provided in the circuit. When the junction temperature exceeds the thermal shutdown temperature, the IC will stop switching. When V_{CC} drops to UVLO, capacitor C_{VCC} will be recharged to the V_{start} level. If the temperature is still too high, V_{CC} will drop again to the UVLO level, etc. (safe restart mode).

Operation recommences when the junction temperature drops 8 degrees typically.

GreenChip™II SMPS control IC

TEA1507

Burst mode standby

Pin CTRL (pin 3) is also used to implement the burst mode standby. In burst mode standby, the power supply enters a special low dissipation state, where it typically consumes less than 1 W of input power ($P_o < 100$ mW), but is still able to supply a microprocessor, for example. Figure 12 shows a flyback converter using the burst mode standby function. The system enters burst mode standby when the microprocessor closes switches S2 and S3 on the secondary side. Switch S2 connects the high voltage output secondary winding to the low voltage microprocessor capacitor ($C_{\mu C}$), bypassing C_o.

When the voltage on $C_{\mu C}$ exceeds the Zener voltage, the opto-coupler is activated, sending a large current signal to CTRL. In response to this signal, the IC stops switching and enters a 'hiccup' mode. This burst activation signal should be present for longer than the 'burst blank' period (typically 30 μs): the blanking time prevents false burst triggering due to spikes. Figure 11 shows the burst-mode standby signals. The hiccup mode during burst mode standby operation does not differ from the hiccup mode in safe-restart mode during a system fault condition (e.g. OVP or output short circuit). The power is reduced during soft-restart mode.

Burst mode standby operation continues until the microcontroller opens switches S2 and S3. The system then enters the start-up sequence and begins normal switching behaviour.

$$I_{burstmode} = \frac{V_{th}}{R_{CTRL}} + I_{th(on)}$$

(For burst mode specification, see Figs 11 and 12.)

Soft start-up (pin I_{sense})

To prevent transformer rattle during hiccup, the transformer peak current is slowly increased by the soft start function. This can be achieved by inserting a resistor and a capacitor between pin I_{sense} (pin 5) and the sense resistor. An internal current source charges the capacitor to $V = I_{ss} \times R_{ss}$, with a maximum of about 0.5 V.

The start level and the time constant of the increasing primary current level can be adjusted externally by changing the values of R_{ss} and C_{ss}.

$$I_{primary(max)} = \frac{V_{ocp} - (I_{ss} \times R_{ss})}{R_{sense}}$$

$$\tau = R_{ss} \times C_{ss}$$

The charging current I_{ss} will flow as long as the voltage on pin I_{sense} is below approximately 0.5 V. If the voltage on pin I_{sense} exceeds the 0.5 V, the soft start current source will start limiting the current I_{ss}. At the $V_{CC(start)}$ level, the I_{ss} current source is completely switched off (see Fig.9).

Since the soft start current I_{ss} is subtracted from pin V_{CC} charging current, the R_{ss} value will affect the V_{CC} charging current level by a maximum of 60 μA (typical value).
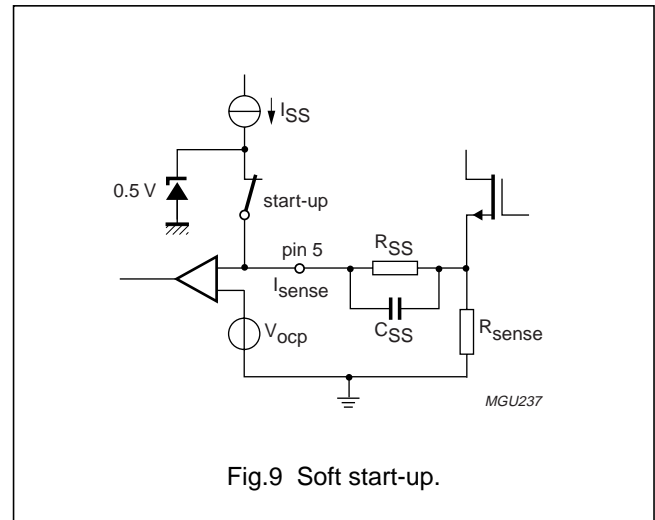
Fig.9 Soft start-up.

Driver

The driver circuit to the gate of the power MOSFET has a current sourcing capability of typically 125 mA and a current sink capability of typical 540 mA. This permits fast turn-on and turn-off of the power MOSFET for efficient operation.

A low driver source current has been chosen to limit the ΔV/Δt at switch-on. This reduces Electro Magnetic Interference (EMI) and also limits the current spikes across R_{sense}.

GreenChip™II SMPS control IC

TEA1507

LIMITING VALUES

In accordance with the Absolute Maximum Rating System (IEC 60134). All voltages are measured with respect to ground (pin 2); positive currents flow into the chip; pin 1 may not be current driven. The voltage ratings are valid provided other ratings are not violated; current ratings are valid provided the maximum power rating is not violated.

SYMBOL	PARAMETER	CONDITIONS	MIN.	MAX.	UNIT
Voltages					
V_1	pin 1 (V_{CC})	continuous	−0.4	+20	V
V_3	pin 3 (CTRL)		−0.4	+5	V
V_4	pin 4 (DEM)	current limited	−0.4	−	V
V_5	pin 5 (I_{sense})	current limited	−0.4	−	V
V_8	pin 8 (DRAIN)		−0.4	+650	V
Currents					
I_3	pin 3 (CTRL)	d < 10%	−	+50	mA
I_4	pin 4 (DEM)		−250	+250	mA
I_5	pin 5 (I_{sense})		−1	+10	mA
I_6	pin 6 (DRIVER)	d < 10%	−0.8	+2	A
I_8	pin 8 (DRAIN)		−	+5	mA
General					
P_{tot}	total power dissipation	T_{amb} < 55 °C	−	1.0	W
T_{stg}	storage temperature		−55	+150	°C
T_{vj}	virtual junction temperature		−20	+145	°C
ESD					
V_{ESD}	electrostatic discharge voltage	class 1			
	human body model	pins 1 to 6; note 1	−	1750	V
		pin 8 (DRAIN); note 1	−	1000	V
	machine model	note 2	−	200	V

Notes

1. Equivalent to discharging a 100 pF capacitor through a 1.5 kΩ series resistor.

2. Equivalent to discharging a 200 pF capacitor through a 0.75 µH coil and a 10 Ω resistor.

THERMAL CHARACTERISTICS

SYMBOL	PARAMETER	CONDITIONS	VALUE	UNIT
$R_{th(j-a)}$	thermal resistance from junction to ambient	in free air; note 1	100	K/W

Note

1. With pin GND connected to sufficient copper area on the printed-circuit board.

QUALITY SPECIFICATION

In accordance with 'SNW-FQ-611-E'.

GreenChip™II SMPS control IC

TEA1507

CHARACTERISTICS

T_{amb} = 25 °C; V_{CC} = 15 V; all voltages are measured with respect to ground (pin 2); currents are positive when flowing into the IC; unless otherwise specified.

SYMBOL	PARAMETER	CONDITIONS	MIN.	TYP.	MAX.	UNIT
Start-up current source (pin 8)						
$I_{i(DRAIN)}$	supply current drawn from drain pin	V_{CC} = 0 V; V_{DRAIN} > 100 V	1.0	1.2	1.4	mA
		with auxiliary supply; V_{DRAIN} > 100 V	–	100	300	µA
BV_{DSS}	breakdown voltage		650	–	–	V
M-level	mains-dependent operation-enabling level		60	–	100	V
V_{CC} management (pin 1)						
$V_{CC(start)}$	start-up voltage on V_{CC}		10.3	11	11.7	V
$V_{CC(UVLO)}$	under voltage lock-out on V_{CC}		8.1	8.7	9.3	V
$V_{CC(hys)}$	hysteresis voltage on V_{CC}	$V_{CC(start)} - V_{CC(UVLO)}$	2.0	2.3	2.6	V
$I_{i(VCC)H}$	pin V_{CC} charging current	V_{DRAIN} > 100 V; V_{CC} < 3V	–1.2	–1	–0.8	mA
$I_{i(VCC)L}$	pin V_{CC} charging current	V_{DRAIN} > 100 V; 3 V < V_{CC} < $V_{CC(UVLO)}$	–1.2	–0.75	–0.45	mA
$I_{VCC(restart)}$	pin V_{CC} restart current	V_{DRAIN} > 100 V; $V_{CC(UVLO)}$ < V_{CC} < $V_{CC(start)}$	–650	–550	–450	µA
$I_{CC(operate)}$	supply current under normal operation	no load on pin DRIVER	1.1	1.3	1.5	mA
Demagnetization management (pin 4)						
V_{DEM}	demagnetization comparator threshold voltage on pin DEM		50	100	150	mV
I_{DEM}	pin DEM current	V_{DEM} = 50 mV	–50[1]	–	0	nA
$V_{clamp(DEM)(neg)}$	negative clamp voltage on pin DEM	at I_{DEM} = –150 µA	–0.5	–0.25	–0.05	V
$V_{clamp(DEM)(pos)}$	positive clamp voltage on pin DEM	at I_{DEM} = 250 µA	0.5	0.7	0.9	V
t_{suppr}	suppression of transformer ringing at start of secondary stroke		1.1	1.5	1.9	µs
Pulse width modulator						
$t_{on(min)}$	minimum on-time		–	t_{leb}	–	ns
$t_{on(max)}$	maximum on-time	latched	40	50	60	µs
Oscillator						
f_{oscL}	oscillator low frequency (fixed frequency)	V_{CTRL} > 1.5 V	5	6.5	8	kHz
f_{oscH}	oscillator high frequency (fixed frequency)	V_{CTRL} < 1 V	145	175	205	kHz
$V_{vco(start)}$	peak voltage at pin I_{sense}, where frequency reduction starts	see Fig.6	–	75	–	mV
$V_{vco(max)}$	peak voltage at pin I_{sense}, where the frequency is equal to f_{oscL}		–	50	–	mV
Duty cycle control (pin 3)						
$V_{CTRL(min)}$	min. voltage on CTRL (max. duty cycle)		–	1.0	–	V
$V_{CTRL(max)}$	max. voltage on CTRL (min. duty cycle)		–	1.5	–	V

GreenChip™II SMPS control IC   TEA1507

SYMBOL	PARAMETER	CONDITIONS	MIN.	TYP.	MAX.	UNIT
Burst mode standby (pin 3)						
$V_{th(burst)(on)}$	burst mode standby active threshold voltage	at I_{burst} = 6 mA	3.3	3.8	4.3	V
$I_{th(burst)(on)}$	burst mode standby active current		16	–	–	mA
$I_{th(burst)(off)}$	burst mode standby inactive current		–	–	6	mA
$t_{(burst-blank)}$	burst mode standby blanking time		25	30	35	µs
Valley switch (pin 8)						
$\Delta V/\Delta t_{valley}$	$\Delta V/\Delta t$ for valley recognition		–85	–	+85	V/µs
$t_{valley-swon}$	delay from valley recognition to switch-on		–	150[1]	–	ns
Current and short winding protection (pin 5)						
$V_{sense(max)}$	maximum source voltage OCP	$\Delta V/\Delta t$ = 0.1 V/µs	0.48	0.52	0.56	V
$t_{propagation}$	delay from detecting $V_{sense(max)}$ to switch-off	$\Delta V/\Delta t$ = 0.5 V/µs	–	140	185	ns
V_{swp}	short winding protection voltage		0.83	0.88	0.96	V
t_{leb}	blanking time for current and short winding protection		300	370	440	ns
I_{ss}	soft start current	V_{sense} < 0.5 V	45	60	75	µA
Overvoltage protection (pin 4)						
$I_{(OVP)(DEM)}$	OVP protection level at pin 4, set by the demagnetization resistor R_{DEM}; see Section "OverVoltage Protection (OVP)"		54	60	66	µA
Overpower protection (pin 4)						
$I_{(OPP)(DEM)}$	OPP current at pin 4, start of OPP correction. Set by the demagnetization resistor R_{DEM}; see Section "OverPower Protection (OPP)"		–	–24	–	µA
$I_{(OPP50\%)(DEM)}$	OPP current at pin 4 where maximum source voltage is limited to 0.3 V		–	–100	–	µA
Driver (pin 6)						
I_{source}	source current capability of driver	V_{CC} = 9.5 V; V_{DRIVER} = 2 V	–	–170	–88	mA
I_{sink}	sink current capability of driver	V_{CC} = 9.5 V; V_{DRIVER} = 2 V	–	300	–	mA
		V_{CC} = 9.5 V; V_{DRIVER} = 9.5 V	400	700	–	mA
$V_{o(driver)(max)}$	maximum output voltage of the driver	V_{CC} > 12 V	–	11.5	12	V
Temperature protection						
$T_{prot(max)}$	maximum temperature threshold		130	140	150	°C
$T_{prot(hyst)}$	hysteresis temperature		–	8[1]	–	°C

Note

1. Guaranteed by design.

GreenChip™II SMPS control IC

TEA1507

APPLICATION INFORMATION

A converter with the TEA1507 consists of an input filter, a transformer with a third winding (auxiliary), and an output stage with a feedback circuit.

Capacitor C_{VCC} (at pin 1) buffers the supply voltage of the IC, which is powered via the high voltage rectified mains during start-up and via the auxiliary winding during operation.

A sense resistor converts the primary current into a voltage at pin I_{sense} (pin 5). The value of this sense resistor defines the maximum primary peak current.

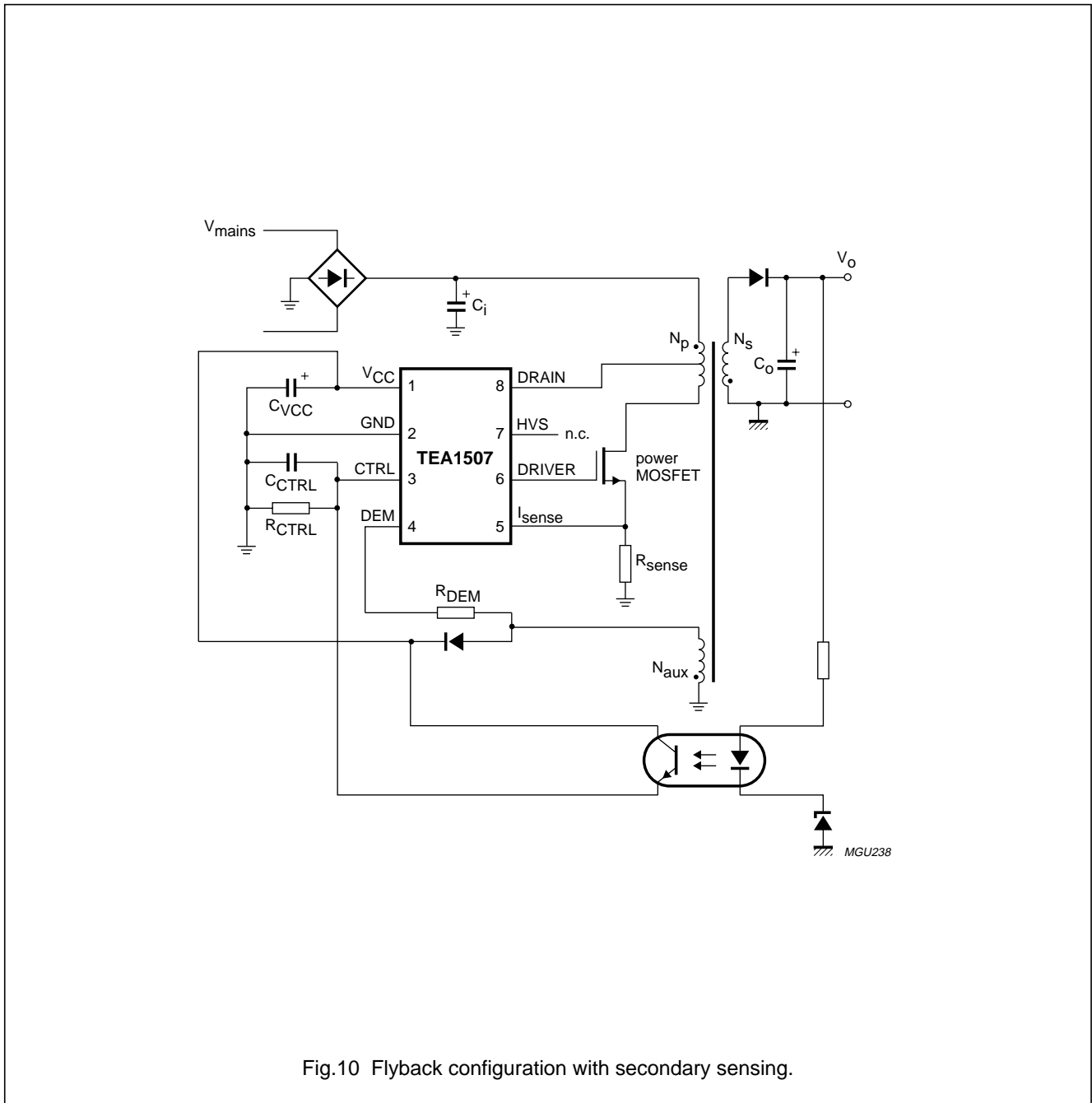An application note is available: AN00047.

Fig.10 Flyback configuration with secondary sensing.
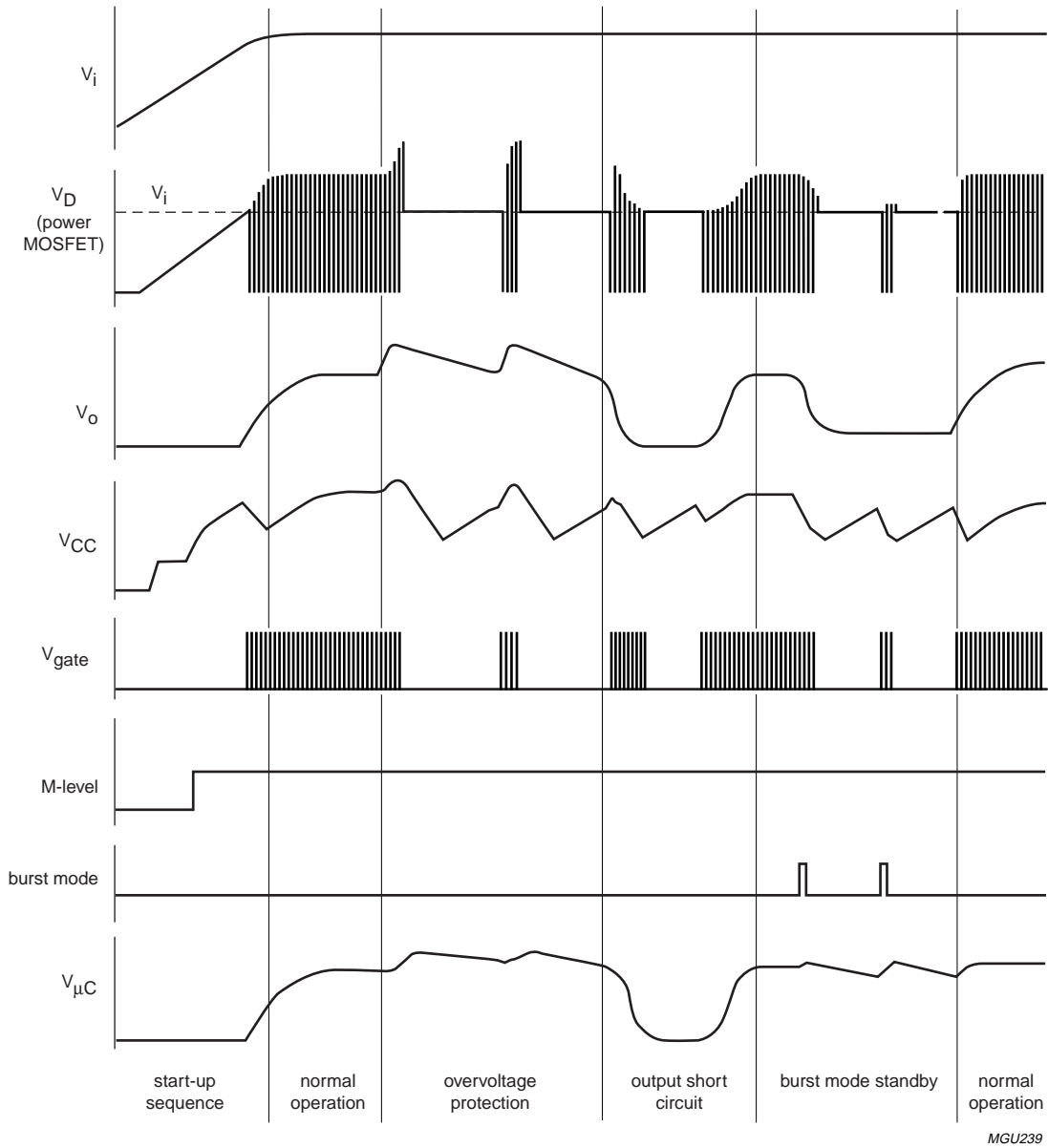
GreenChip™II SMPS control IC
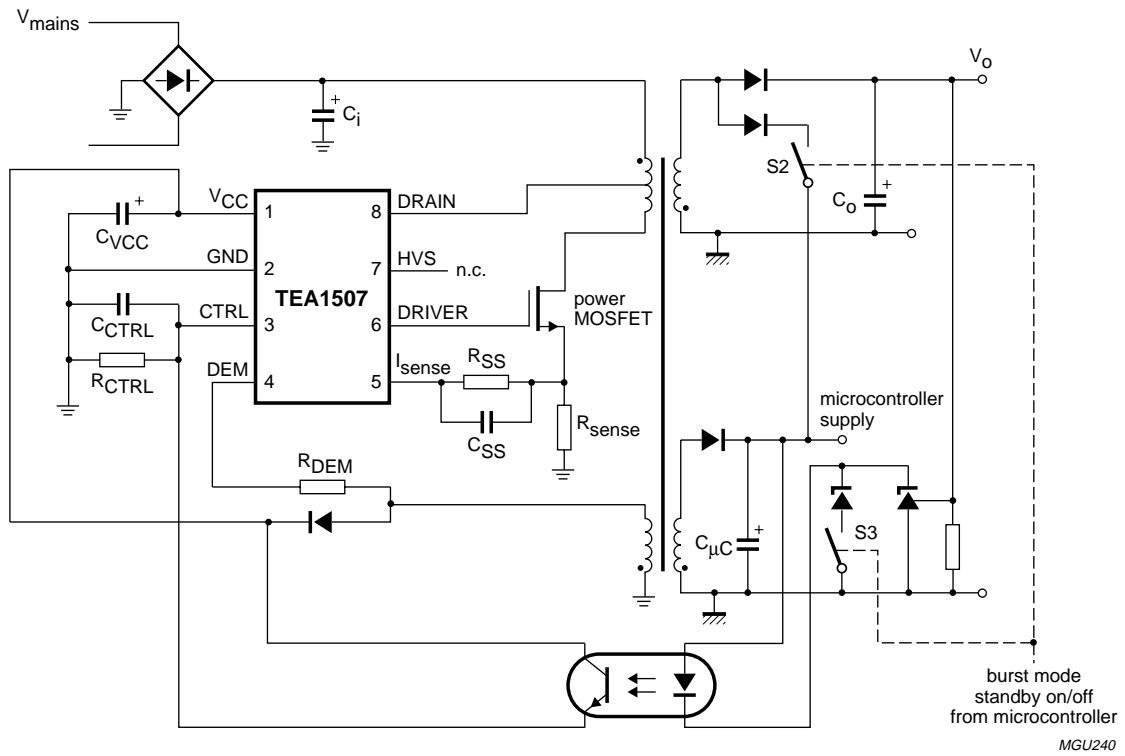
TEA1507

Fig.11 Typical waveforms.

Fig.12 Flyback configuration with secondary sensing using the burst mode standby.

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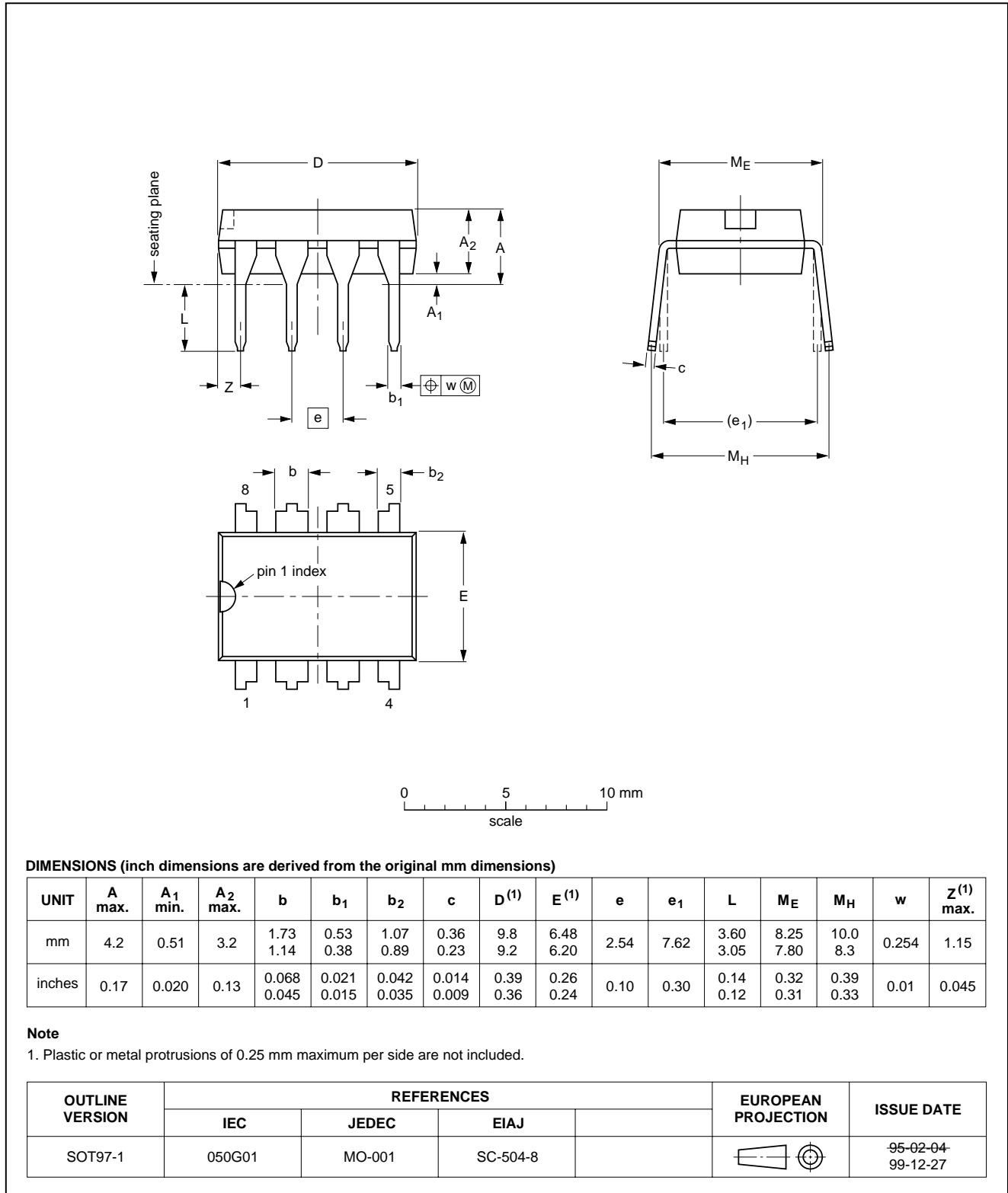TEA1507

PACKAGE OUTLINE

DIP8: plastic dual in-line package; 8 leads (300 mil)

SOT97-1

DIMENSIONS (inch dimensions are derived from the original mm dimensions)

UNIT	A max.	A$_1$ min.	A$_2$ max.	b	b$_1$	b$_2$	c	D$^{(1)}$	E$^{(1)}$	e	e$_1$	L	M$_E$	M$_H$	w	Z$^{(1)}$ max.
mm	4.2	0.51	3.2	1.73 1.14	0.53 0.38	1.07 0.89	0.36 0.23	9.8 9.2	6.48 6.20	2.54	7.62	3.60 3.05	8.25 7.80	10.0 8.3	0.254	1.15
inches	0.17	0.020	0.13	0.068 0.045	0.021 0.015	0.042 0.035	0.014 0.009	0.39 0.36	0.26 0.24	0.10	0.30	0.14 0.12	0.32 0.31	0.39 0.33	0.01	0.045

Note

1. Plastic or metal protrusions of 0.25 mm maximum per side are not included.

OUTLINE VERSION	REFERENCES				EUROPEAN PROJECTION	ISSUE DATE
	IEC	JEDEC	EIAJ			
SOT97-1	050G01	MO-001	SC-504-8			~~95-02-04~~ 99-12-27

GreenChip™II SMPS control IC   TEA1507

SOLDERING

Introduction to soldering through-hole mount packages

This text gives a brief insight to wave, dip and manual soldering. A more in-depth account of soldering ICs can be found in our *"Data Handbook IC26; Integrated Circuit Packages"* (document order number 9398 652 90011).

Wave soldering is the preferred method for mounting of through-hole mount IC packages on a printed-circuit board.

Soldering by dipping or by solder wave

The maximum permissible temperature of the solder is 260 °C; solder at this temperature must not be in contact with the joints for more than 5 seconds.

The total contact time of successive solder waves must not exceed 5 seconds.

The device may be mounted up to the seating plane, but the temperature of the plastic body must not exceed the specified maximum storage temperature ($T_{stg(max)}$). If the printed-circuit board has been pre-heated, forced cooling may be necessary immediately after soldering to keep the temperature within the permissible limit.

Manual soldering

Apply the soldering iron (24 V or less) to the lead(s) of the package, either below the seating plane or not more than 2 mm above it. If the temperature of the soldering iron bit is less than 300 °C it may remain in contact for up to 10 seconds. If the bit temperature is between 300 and 400 °C, contact may be up to 5 seconds.

Suitability of through-hole mount IC packages for dipping and wave soldering methods

PACKAGE	SOLDERING METHOD	
	DIPPING	WAVE
DBS, DIP, HDIP, SDIP, SIL	suitable	suitable[1]

Note

1. For SDIP packages, the longitudinal axis must be parallel to the transport direction of the printed-circuit board.

GreenChip™II SMPS control IC

TEA1507

DATA SHEET STATUS

DATA SHEET STATUS	PRODUCT STATUS	DEFINITIONS [1]
Objective specification	Development	This data sheet contains the design target or goal specifications for product development. Specification may change in any manner without notice.
Preliminary specification	Qualification	This data sheet contains preliminary data, and supplementary data will be published at a later date. Philips Semiconductors reserves the right to make changes at any time without notice in order to improve design and supply the best possible product.
Product specification	Production	This data sheet contains final specifications. Philips Semiconductors reserves the right to make changes at any time without notice in order to improve design and supply the best possible product.

Note

1. Please consult the most recently issued data sheet before initiating or completing a design.

DEFINITIONS

Short-form specification — The data in a short-form specification is extracted from a full data sheet with the same type number and title. For detailed information see the relevant data sheet or data handbook.

Limiting values definition — Limiting values given are in accordance with the Absolute Maximum Rating System (IEC 60134). Stress above one or more of the limiting values may cause permanent damage to the device. These are stress ratings only and operation of the device at these or at any other conditions above those given in the Characteristics sections of the specification is not implied. Exposure to limiting values for extended periods may affect device reliability.

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